



FAN LAWS – Changing Fan RPM on a Given Fan System

$$CFM_2 = CFM_1 \times \left(\frac{RPM_2}{RPM_1} \right)$$

$$SP_2 = SP_1 \times \left(\frac{RPM_2}{RPM_1} \right)^2$$

$$HP_2 = HP_1 \times \left(\frac{RPM_2}{RPM_1} \right)^3$$

1 = Initial; 2 = Desired

MOTOR HEAT

$$BTUH = BHP \times 2547 \div \text{Efficiency}$$

FAN HORSEPOWER

$$BHP = \frac{CFM \times \text{Static Pressure (Inches)}}{6356 \times \text{Static Efficiency}}$$

MOTOR ELECTRICAL CALCULATIONS

ALL MOTORS

$$KW \text{ Input} = \frac{BHP \times .746}{\text{Efficiency}}$$

SINGLE PHASE MOTORS

$$KW = \frac{AMPS \times Volts \times \text{Power Factor}}{1000}$$

$$AMPS = \frac{746 \times BHP}{\text{Efficiency} \times Volts \times \text{Power Factor}}$$

THREE PHASE MOTORS

$$KW = \frac{AMPS \times Volts \times 1.732 \times P.F.}{1000}$$

$$AMPS = \frac{746 \times BHP}{\text{Efficiency} \times Volts \times P.F. \times 1.732}$$

ELECTRIC HEAT CALCULATIONS

$$1 \text{ kW} = 3,413 \text{ BTUH} / \text{kW} = 3.413 \text{ MBH}$$

$$LAT = \frac{\text{Heater kW} \times 3,413 \text{ BTUH} / \text{kW}}{1.08^* \times \text{SCFM}} + \text{EAT}$$

* Air density at sea level. Reduce by 0.036 for each 1000 feet of altitude above sea level.

LAT = Leaving Air Temperature

EAT = Entering Air Temperature

Heaters > 48 AMPS are subdivided and fused

HEATER AMP CALCULATION	
VOLTAGE	AMPS per kW
115/1	8.70
120/1	8.33
208/1	4.81
230/1	4.35
240/1	4.17
277/1	3.61
208/3	2.78
230/3	2.51
240/3	2.41
460/3	1.26
480/3	1.20
575/3	1.00
600/3	.962

CAPACITY CALCULATIONS

$$1 \text{ Ton} = 12,000 \text{ BTUH}$$

For Glycol: 20% use 475, 30% use 464, 40% use 449, 50% use 433

$$\text{Water Side (no glycol) BTUH} = 500 \times \text{GPM} \times \Delta T$$

$$\text{Sensible Heat BTUH} = 1.08 \times \text{CFM} \times \Delta T \times \text{ADR}^*$$

$$\text{Latent Heat BTUH} = 0.68 \times \text{CFM} \times \text{Grain Difference} \times \text{ADR}^*$$

$$\text{Total Heat BTUH} = 4.5 \times \text{CFM} \times \text{Enthalpy Difference} \times \text{ADR}^*$$

$$\text{Pressure of Water in Feet} = 2.31 \times \text{PSI}$$

$$\text{Pump Horsepower BHP} = \frac{\text{GPM} \times \text{Head in Feet}}{\text{Density Ratio}}$$

$$\Delta \text{PSIG} = \left(\frac{\text{GPM}}{C_V} \right)^2 \times 3960 \times \text{Pump Efficiency}$$

Altitude	Air Density Ratio at 70°F Air Temp.
2000	.930
4000	.864
6000	.801
8000	.743

AIR BALANCING

$$V = \text{CFM} \div \text{Area} \quad P_V = \left(V \div 4005 \right)^2$$

$$P_S = P_T - P_V \text{ (inches of water column)}$$

V = Velocity (fpm). P_V = Velocity Pressure. P_S = Static Pressure. P_T = Total Pressure.

PRESSURE DROP FOR VALVE PACKAGE COMPONENTS

$$(\text{GPM} \div C_V \text{ Ball Valve})^2 \times (\text{Qty. of Ball Valves}) + (\text{GPM} \div C_V \text{ Strainer})^2 +$$

$$(\text{GPM} \div C_V \text{ Flow Control})^2 + (\text{GPM} \div C_V \text{ Control Valve})^2$$

= Pressure Drop (PSI)

CHANGING WATER FLOW IN A GIVEN CLOSED PIPING SYSTEM

$$PD_2 = PD_1 \left(\frac{\text{GPM}_2}{\text{GPM}_1} \right)^2 \quad 1 = \text{Initial}; 2 = \text{Desired}$$